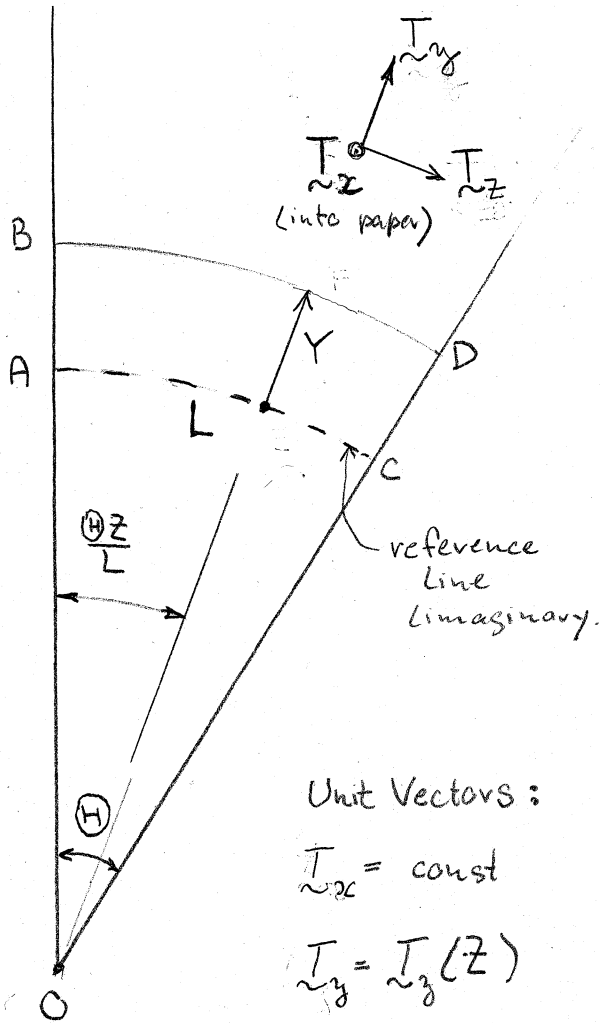


Generalized Plane Strain Formulation (melint 13)

(X, Y, Z) Material Coordinates



Unit Vectors:

$$\underline{T}_x = \text{const}$$

$$\underline{T}_y = \underline{T}_y(Z)$$

$$\underline{T}_z = \underline{T}_z(Z)$$

Undeformed Configuration

$$\underline{T}_{y,z} = \frac{\Theta}{L} \underline{T}_z \quad \underline{T}_{z,z} = -\frac{\Theta}{L} \underline{T}_y$$

$$\underline{R} = X \underline{T}_x + \left(Y + \frac{L}{\Theta} \right) \underline{T}_y$$

$$\underline{R}_{,X} = \underline{T}_x$$

$$\underline{R}_{,Y} = \underline{T}_y$$

$$\underline{R}_{,Z} = \left(Y + \frac{L}{\Theta} \right) \frac{\Theta}{L} \underline{T}_z$$

$$= \left(\frac{Y\Theta}{L} + 1 \right) \underline{T}_z$$

Unit Vectors

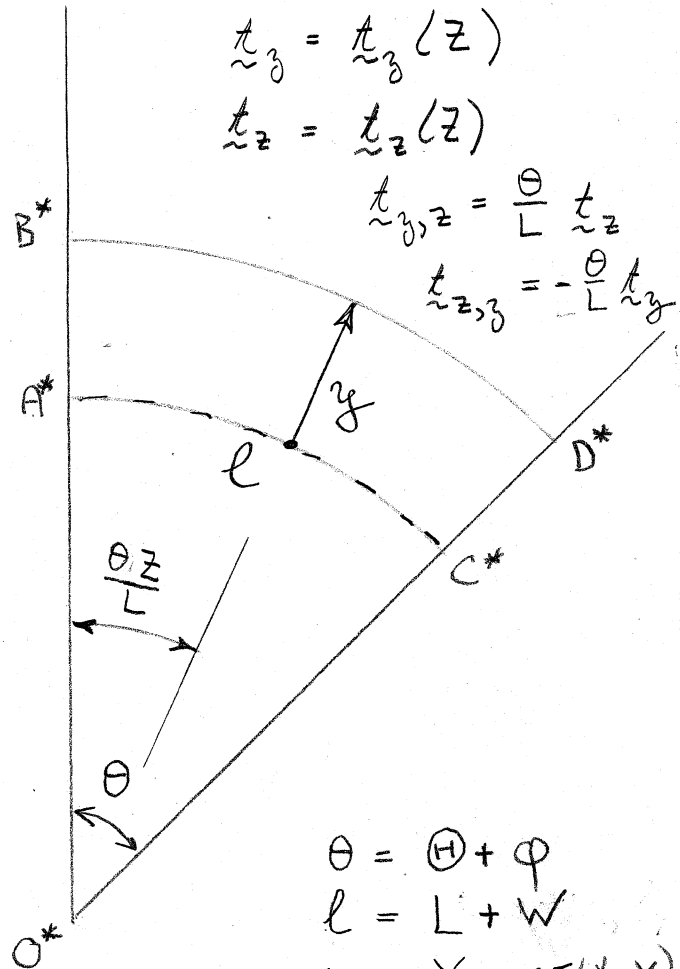
$$\underline{t}_x = \underline{T}_x \text{ (const.)}$$

$$\underline{t}_y = \underline{t}_y(Z)$$

$$\underline{t}_z = \underline{t}_z(Z)$$

$$\underline{t}_{y,z} = \frac{\Theta}{L} \underline{t}_z$$

$$\underline{t}_{z,z} = -\frac{\Theta}{L} \underline{t}_y$$



$$\theta = \Theta + \varphi$$

$$l = L + W$$

$$y = Y + v(x, Y)$$

$$x = X + u(x, Y)$$

Deformed Configuration

$$\underline{r} = x \underline{t}_x + \left(y + \frac{l}{\Theta} \right) \underline{t}_y$$

$$\underline{r}_{,x} = x_{,x} \underline{t}_x + v_{,x} \underline{t}_y$$

$$\underline{r}_{,Y} = y_{,Y} \underline{t}_y + u_{,Y} \underline{t}_x$$

$$\underline{r}_{,Z} = \left(y + \frac{l}{\Theta} \right) \frac{\Theta}{L} \underline{t}_z$$

$$= \left(\frac{l}{L} + \frac{y\Theta}{L} \right) \underline{t}_z$$

Undeformed Config

Length of fiber :

$$A_z = L + Y \Theta$$

$$\underline{G}_x = \underline{R}_{,x} = \underline{I}_x$$

$$\underline{G}_y = \underline{R}_{,y} = \underline{I}_y$$

$$\underline{G}_z = \underline{R}_{,z} = (A_z/L) \underline{I}_z$$

$$\underline{G}^x = \underline{I}_x$$

$$\underline{G}^y = \underline{I}_y$$

$$\underline{G}^z = (L/A_z) \underline{I}_z$$

Deformed Config

$$a_z = l + y \Theta$$

$$\underline{g}_x = x_{,x} \underline{t}_x + v_{,x} \underline{t}_y$$

$$\underline{g}_y = y_{,y} \underline{t}_y + u_{,y} \underline{t}_x$$

$$\underline{g}_z = (a_z/L) \underline{t}_z$$

$$\underline{g}^z = (L/a_z) \underline{t}_z$$

Def. Gradient Tensor

$$\underline{\underline{F}} = \underline{\underline{r}}_{,x} \underline{\underline{T}}_x + \underline{\underline{r}}_{,y} \underline{\underline{T}}_y + \underline{\underline{r}}_{,z} \left((L/A_z) \underline{\underline{T}}_z \right)$$

Green Lagr. Strain Tensor : $(2\underline{\underline{E}} = \underline{\underline{F}}^T \cdot \underline{\underline{F}} - \underline{\underline{1}})$

$$\underline{\underline{E}} = E_{xx} \underline{\underline{T}}_x \underline{\underline{T}}_x + E_{yy} \underline{\underline{T}}_y \underline{\underline{T}}_y + E_{xy} (\underline{\underline{T}}_x \underline{\underline{T}}_y + \underline{\underline{T}}_y \underline{\underline{T}}_x) \\ + E_{zz} \underline{\underline{T}}_z \underline{\underline{T}}_z$$

$$E_{xx} = u_{,x} + \frac{1}{2} (u_{,x}^2 + v_{,x}^2)$$

$$E_{yy} = v_{,y} + \frac{1}{2} (u_{,y}^2 + v_{,y}^2)$$

$$2 E_{xy} = u_{,y} + v_{,x} + u_{,x} u_{,y} + v_{,x} v_{,y}$$

$$E_{zz} = \frac{1}{2} \left(1 + \frac{\Theta}{L} Y \right)^{-2} \left\{ \underline{\underline{r}}_{,z} \cdot \underline{\underline{r}}_{,z} - \left(1 + \frac{\Theta}{L} Y \right)^2 \right\}$$

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$$E_{zz} = \frac{1}{2} (L + \Theta Y)^{-2} \left\{ (l + \Theta y)^2 - (L + \Theta Y)^2 \right\}$$

$$\text{Let } \begin{cases} A_z = L + \Theta Y (=BD) \\ a_z = l + \Theta y (=B^*D^*) \end{cases} \quad E_{zz} = \frac{1}{2} \left(\frac{a_z^2 - A_z^2}{A_z^2} \right)$$

$$\begin{aligned} a_z &= L + W + (\Theta + \varphi)(Y + v) \\ &= L + \Theta Y + W + \Theta v + \varphi(Y + v) \\ &= A_z + W + \Theta v + \varphi Y \end{aligned}$$

$$\Rightarrow E_{zz} = \epsilon_z + \frac{1}{2} \epsilon_z^2, \quad \epsilon_z = \frac{W + \Theta v + \varphi Y}{A_z}$$

$$A_z = L + \Theta Y$$

$$dV = A_z dX dY \quad (\text{undeformed volume element})$$

$$\delta E_{zz} = \frac{a_z}{A_z^2} \delta a_z = \frac{a_z}{A_z^2} (\delta W + \delta \varphi Y + \Theta \delta v)$$

$$\begin{aligned} \delta_1 \delta_2 E_{zz} &= \frac{1}{A_z^2} (\delta_1 a_z \delta_2 a_z + a_z \delta_1 \delta_2 a_z) \\ &= \frac{1}{A_z^2} [(\delta_1 W + Y \delta_1 \varphi + \Theta \delta_1 v)(\delta_2 W + Y \delta_2 \varphi + \Theta \delta_2 v) \\ &\quad + a_z (\delta_1 v \delta_2 \varphi + \delta_2 v \delta_1 \varphi)] \end{aligned}$$

To interpret the applied forces corresponding to w & ϕ Consider EVW for system of External Applied Forces in Equilibrium for virtual displacements δw & $\delta \phi$:

Virtual Displ δw

$$l = L + w \Rightarrow \delta l = \delta w$$

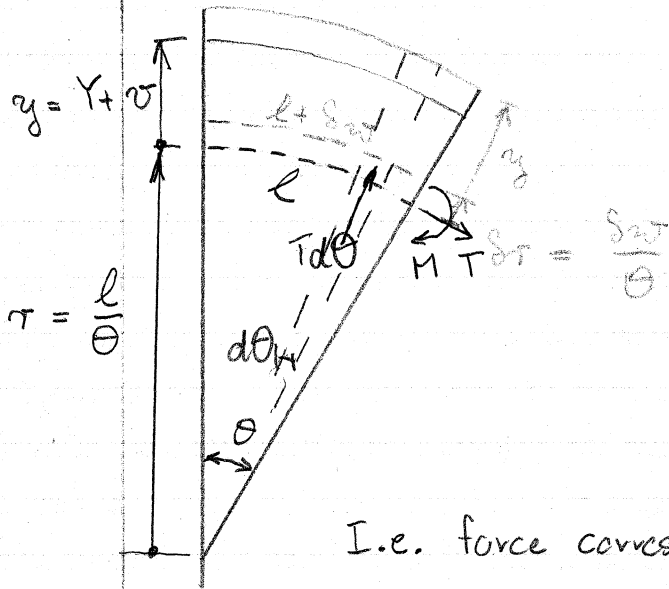
$$\theta = \Theta + \phi \Rightarrow \delta \theta = \delta \phi$$

Ext. Virt. Wk.

$$EVW = \frac{\delta w}{\theta} \int T d\theta = T \delta w$$

Note: for syst in equil., rigid body displ & rot. may always be added in evaluating Ext. Virt. wk.

I.e. force corresponding to w is the axial tension.



Virt. Displ. $\delta \phi$

$$\delta \theta = \delta \phi, \quad r_r = - \frac{l \delta \phi}{\theta^2}$$

$$EVW = M \delta \phi$$

$$+ T r_r \delta \phi$$

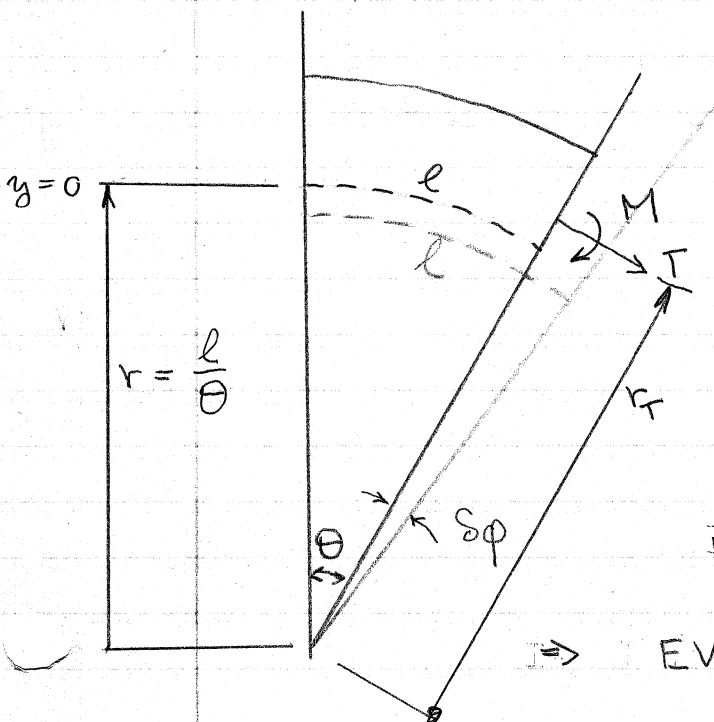
$$- \int \frac{l \delta \phi}{\theta^2} \int T d\theta$$

$$EVW = \{ M + T(r_r - r) \} \delta \phi$$

$$\text{where } r_r = r + y_r$$

$$\Rightarrow EVW = (M + y_r T) \delta \phi$$

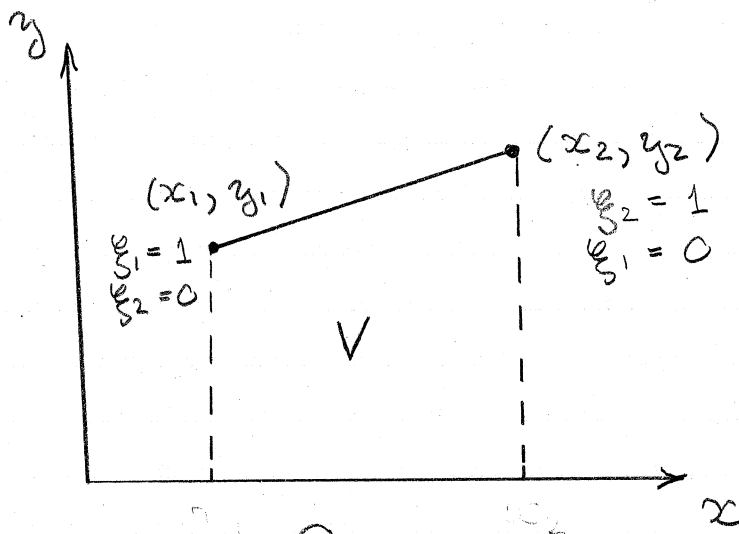
$$[y_r = y \text{ coordinate of point where}]$$



Pressure Loads Incl End Caps

With ref. to p.1 the area $A^*C^*D^*B^*$ is

$$\begin{aligned}
 A &= \frac{1}{2} \theta [(O^*B^*)^2 - (O^*A^*)^2] \\
 &= \frac{1}{2} \theta [(r+y)^2 - r^2] \quad , \quad r = O^*A^* \\
 &= \theta r y + \frac{1}{2} \theta y^2 = l y + \frac{1}{2} \theta y^2
 \end{aligned}$$



$$\begin{aligned}
 V &= \int_{\textcircled{1}}^{\textcircled{2}} A dx \quad , \quad x = \xi_1 x_1 + \xi_2 x_2 \\
 y &= \xi_1 y_1 + \xi_2 y_2 \\
 \xi_1 + \xi_2 &= 1 \\
 \xi_2 &= \xi \quad , \quad \text{say}
 \end{aligned}$$

$$\begin{aligned}
 V &= \int_0^1 (l y + \frac{1}{2} \theta y^2) x_{12} d\xi \quad , \quad x_{12} = x_2 - x_1 \\
 &= \int_0^1 \left\{ l [\xi_1 y_1 + \xi_2 y_2] + \frac{1}{2} \theta [\xi_1 y_1 + \xi_2 y_2]^2 \right\} x_{12} d\xi_2 \\
 &= \left\{ \frac{1}{2} l (y_1 + y_2) + \frac{1}{6} \theta (y_1^2 + y_1 y_2 + y_2^2) \right\} x_{12}
 \end{aligned}$$

Let $y_{av} = \frac{1}{2}(y_1 + y_2)$

$$y_{ms} = \frac{1}{3}(y_1^2 + y_1 y_2 + y_2^2)$$

$$\frac{\partial y_{av}}{\partial y_d} = \frac{1}{2} \quad (d = 1, 2)$$

$$\frac{\partial y_{ms}}{\partial y_d} = b_d, \quad b_1 = \frac{1}{3}(2y_1 + y_2), \quad b_2 = \frac{1}{3}(2y_2 + y_1)$$

$$V = \left(l y_{av} + \frac{1}{2} \theta y_{ms} \right) x_{12}$$

$$\frac{\partial V}{\partial x_{12}} = l y_{av} + \frac{1}{2} \theta y_{ms}$$

$$\frac{\partial V}{\partial y_d} = \frac{1}{2} (l + \theta b_d) x_{12}$$

$$\frac{\partial V}{\partial l} = y_{av} x_{12}$$

$$\frac{\partial V}{\partial \theta} = \frac{1}{2} y_{ms} x_{12}$$

$$\text{Let } \underline{x} = [x_{12} \quad y_1 \quad y_2 \quad l \quad \theta]^T$$

$$\frac{\partial V}{\partial \underline{x}} = \begin{bmatrix} l y_{av} + \frac{1}{2} \theta y_{ms} \\ \frac{1}{2} (l + \theta b_1) x_{12} \\ \frac{1}{2} (l + \theta b_2) x_{12} \\ y_{av} x_{12} \\ \frac{1}{2} y_{ms} x_{12} \end{bmatrix}$$

$$\frac{\partial^2 V}{\partial \underline{x} \partial \underline{x}^T} = \begin{bmatrix} 0 & \frac{1}{2} (l + \theta b_1) & \frac{1}{2} (l + \theta b_2) & y_{av} & \frac{1}{2} y_{ms} \\ \frac{1}{2} (l + \theta b_1) & \frac{1}{3} \theta x_{12} & \frac{1}{6} \theta x_{12} & \frac{1}{2} x_{12} & \frac{1}{2} b_1 x_{12} \\ \frac{1}{2} (l + \theta b_2) & \frac{1}{6} \theta x_{12} & \frac{1}{3} \theta x_{12} & \frac{1}{2} x_{12} & \frac{1}{2} b_2 x_{12} \\ y_{av} & \frac{1}{2} x_{12} & \frac{1}{2} x_{12} & 0 & 0 \\ \frac{1}{2} y_{ms} & \frac{1}{2} b_1 x_{12} & \frac{1}{2} b_2 x_{12} & 0 & 0 \end{bmatrix}$$

E.g. for $x_{12} = 4$, $y_1 = 5$, $y_2 = 8$, $\theta = .3$, $l = 10$,
(ref ma25)

$$\frac{\partial V}{\partial \underline{x}} = \begin{bmatrix} 71.45 \\ 23.6 \\ 24.2 \\ 26 \\ 86 \end{bmatrix}$$

$$\frac{\partial^2 V}{\partial \underline{x} \partial \underline{x}^T} = \begin{bmatrix} 0 & 5.9 & 6.05 & 6.5 & 21.5 \\ 5.9 & 0.4 & 0.2 & 2 & 12 \\ 6.05 & 0.2 & 0.4 & 2 & 14 \\ 6.5 & 2 & 2 & 0 & 0 \\ 21.5 & 12 & 14 & 0 & 0 \end{bmatrix}$$

For positive pressure p acting from left to right when looking from node 1 towards node 2, the potential of the pressure load is

$$\pi = pV$$

$$p^{(e)} = -\pi_{,q} = -p \begin{bmatrix} V_{,x_{12}} \\ V_{,y_1} \\ V_{,x_{12}} \\ V_{,y_2} \\ V_{,l} \\ V_{,\theta} \end{bmatrix} \quad k^{(e)} = p \begin{bmatrix} V_{,x_{12}x_{12}} & -V_{,x_{12}y_1} & -V_{,x_{12}x_{12}} \\ -V_{,y_1x_{12}} & V_{,y_1y_1} & -V_{,y_1x_{12}} \\ -V_{,x_{12}x_{12}} & V_{,x_{12}y_1} & V_{,x_{12}x_{12}} \\ -V_{,y_2x_{12}} & V_{,y_2y_1} & V_{,y_2x_{12}} \\ -V_{,lx_{12}} & V_{,ly_1} & V_{,lx_{12}} \\ -V_{,\theta x_{12}} & V_{,\theta y_1} & V_{,\theta x_{12}} \end{bmatrix} \text{ etc.}$$

$$q = [u_1 \quad v_1 \quad u_2 \quad v_2 \quad W \quad \phi]^T$$

Body Force

Force per unit undeformed volume:

$$\underline{b} = b_x \underline{\hat{t}}_x + b_y \underline{\hat{t}}_y + b_z \underline{\hat{t}}_z \quad . \text{ Assume } b_z = 0.$$

Virtual Displ.

$$\begin{aligned} \delta \underline{u} = & \delta u \underline{\hat{t}}_x + \left(\delta v + \frac{\delta W}{\theta} - \frac{\ell}{\theta^2} \delta \phi \right) \underline{\hat{t}}_y \\ & + \left(y + \frac{\ell}{\theta} \right) \underline{\hat{t}}_z \frac{z}{L} \delta \phi \end{aligned}$$

Virt. Work per unit undeformed Volume:

$$\begin{aligned} \delta W_e &= \underline{b} \cdot \delta \underline{u} \\ &= b_x \delta u + b_y \left(\delta v + \frac{\delta W}{\theta} - \frac{\ell}{\theta^2} \delta \phi \right) \end{aligned}$$

$$dV = A_z dx dy \quad A_z = L + (\theta) Y$$

$$= A_z \text{Det} \left(\frac{d\underline{x}}{d\underline{\xi}} \right) d\xi dy$$

Total Ext. Virt Wk.

$$\begin{aligned} EVW = & \int_{x,y} (b_x \delta u + b_y \delta v) A_z dx dy \\ & + \left(\frac{\delta W}{\theta} - \frac{\ell}{\theta^2} \delta \phi \right) \int_{x,y} b_y A_z dx dy \end{aligned}$$

Leave out 2nd term. At most this affects the interpretation of the nodal forces corresponding to w & ϕ . Indeed omitting this term, it remains that these must be the axial tension T acting at $y=0$ and moment M , from p.4, respectively. Thus use

$$\begin{aligned} EVW &= \int (b_x \delta u + b_y \delta v) A_z \text{Det}(\underline{J}) d\xi d\eta \\ &\approx \sum_{i=1}^4 (b_x \delta u_i + b_y \delta v_i) A_z \text{Det}(\underline{J}) \\ &\quad \text{for single int. pt. in middle} \end{aligned}$$